

DOWNTOWN EAST



PRESENTED BY



Ryan Bonniwell Partner









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MSFA RAMP



MILLWRIGHT BUILDING



WELLS FARGO OFFICES





TEAM

- ARCHITECT: RYAN A+E
- GENERAL CONTRACTOR: RYAN COMPANIES
- STEEL FABRICATOR: LEJEUNE STEEL

HIGHLIGHTS

- Two 17-story office buildings totaling 1.2 Million SF
- Part of 5-block development including retail, hotel, residential and park
- Skyway connection from US Bank Stadium to Downtown
- Total development cost of \$700 Million

























STRUCTURAL SYSTEM ROCK ANCHOR INSTALLATION







FLOOR LEVELNESS





Who wants level floors?

- Owners
- Architects
- Contractors
- Us

Everyone but the gypcrete supplier.



UN-LEVEL ISSUES



- Moveable partitions
- Sliding doors
- Glass handrails
- Furniture
- Finishes

Anything designed with less than ½" of adjustability







LEVELNESS VS FLATNESS FF/FL

"Flatness can be described as bumpiness of the floor and is the degree to which a floor surface is smooth or plane. Levelness is the degree to which a floor surface parallels the slope established on the project drawings."

- ACI 117-06 Tolerances for Concrete Construction









COMPOSITE FLOORS



Why is levelness not applicable?

- Steel tolerances
 - fabrication,
 - erection,
 - camber
- Environmental conditions
- Material Variability
- Concrete placement method
- Concrete Shrinkage
- DEFLECTION



NOTE ON TOLERANCE



Camber is measured with beam laid flat in the shop

- 45ft beam specified with 3" camber could have as little as 2 ¼" within tolerance
- Vertical erection tolerance at beam connection is 3/8

- 6.4.4. For beams that are specified in the contract documents with camber, beams received by the fabricator with 75% of the specified camber shall require no further cambering. Otherwise, the variation in camber shall be as follows:
 - (a) For beams that are equal to or less than 50 ft [15 000 mm] in length, the variation shall be equal to or less than minus zero / plus ½ in. [13 mm].
 - (b) For beams that are greater than 50 ft [15 000 mm] in length, the variation shall be equal to or less than minus zero / plus ½ in. plus ½ in. for each 10 ft or fraction thereof [13 mm plus 3 mm for each 3 000 mm or fraction thereof] in excess of 50 ft [15 000 mm] in length.

For the purpose of inspection, camber shall be measured in the fabricator's shop in the unstressed condition.

Commentary:

There is no known way to inspect beam camber after the beam is received in the field because of factors that include:

- (a) The release of stresses in members over time and in varying applications;
- (b) The effects of the dead weight of the member;
- (c) The restraint caused by the end convections in the crected state; and,
- (d) The effects of additional dead load that may ultimately be intended to be applied, if any.

Therefore, inspection of the *fabricator's* work on beam camber must be done in the fabrication shop in the unstressed condition.









FLOORFRAMNG

Wells Fargo – Downtown East

- 30' x 47'-32'-47'
- Adjusted Camber at columns
- Decided to polish floors after they were mostly poured







ADJUSTING CAMBER

- Purlins that frame to columns are shorter by the column depth than mid-bay purlins (14 ½" for W14x120 – 20 ¼" for W14x550)
- Connections are typically shear tabs or single angles at girders, double angles at columns
- Stiffness of supporting member restrains end rotation







ADJUSTING CAMBER

Deflection Calcs for 47ft purlin

Mid-Bay: $\Delta = 3.194$ " (initial load)

 \square Col (W14x120) $\Delta = 2.878$ " (initial load)

Change of 5/16" (10%)



Contribution of connection and backup member is difficult to calculate and connection is typically deferred. Experience shows that this reduces the deflection by about 20% relative to a mid-bay purlin.

The result is a +/- 30% reduction in camber at the columns, or about 1" on a 45ft bay.

OUTCOMES

Steel was surveyed before and after pour, along with top of slab elevation in two test bays.

Top of slab elevations were generally within ½" and after the first two floors, the surveys were not performed.







OUTCOMES - LONG TERM

During construction of Millwright, WF build-out occurred at Skyway Level

(21 months after slab pour) Long-term deflections of ½" to 1" Millwright Surveyed at 180 days and found ½" – ¾"











Figure 4.E5 Shrinkage Deflection of Composite Beams (by analysing the structure as an eccentrically loaded column)

Shrinkage effect on composite beams

- Shrinkage is variable
- Deck restrains free shrinkage by about 25%
- 1/3 of shrinkage occurs in first month, 90% in first year
- Typically assume $\varepsilon = 0.0003$

For 45' purlin, $\Delta sh = 1/2$ " (+/- 15% of $\Delta initial - L/1100$) For 30' purlin, $\Delta sh = 5/16$ " (+/- 15% of $\Delta initial - L/1100$)



Design Guide 36 Design Considerations for Camber







RECOMMENDATIONS



- Have early discussions with the design team and construction team
- Understand and communicate owner expectations
- Identify floor finish early and understand impact
- Discuss potential costs and savings
- Ask contractor what they believe is achievable
- Test camber at the shop and survey steel prior to pour to head off potential issues

RECOMMENDATIONS



For uniform thickness slab (generally lowest up-front cost)

- Screed from cambered beams
- Camber for 115% DL (based on shrinkage calc)
- Design steel for specified slab thickness + construction LL
- Adjust camber at purlins framing to column flanges







COLUMN SHORTENING

RYA





COLUMN SHORTENING





The Banging Bold Syndrome:

Unexpected loud noises can cause high anxiety for building owners and tenants

- Beam is not truly simply-supported
- Shrinkage acts along the length of the building
- Bolts designed for bearing are torqued to the level that creates friction between the beam web and connection (more than "snug tight"
- When shrinkage strains build to a level that overcomes the friction, the result is a sudden release of energy as the bolt slips, creating a loud "bang"
- Unsettling but not structurally concerning



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STRUCTURAL ENGINEERING



